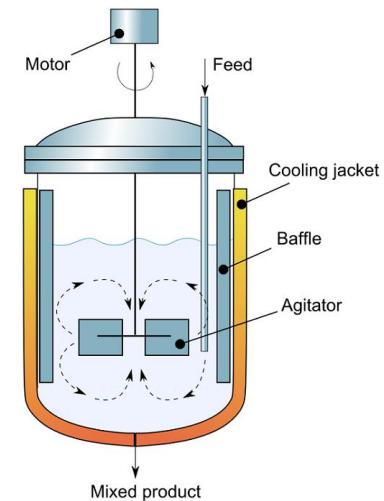
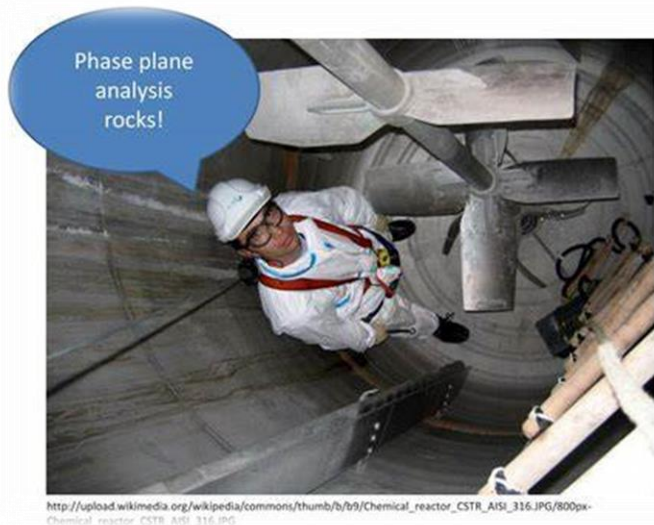


Reactor Design II



Week 9

CSTR With Heat Effects

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Introduction

- Chemical Reaction Engineering (CRE) explores reactor design, including heat effects and stability.
- This lecture focuses on Continuous Stirred Tank Reactors (CSTRs) with heat effects, multiple steady states, and the concepts of ignition and extinction temperatures.

Topics to be Addressed

- - Fundamentals of CSTR with Heat Effects
- - Unsteady-State and Steady-State Energy Balances
- - Multiple Steady States (MSS): Analysis and Stability
- - Ignition and Extinction Temperatures
- - Practical Examples and Case Studies

Objectives

- By the end of this lecture, students will be able to:
 - - Understand heat effects in CSTR operation.
 - - Analyze unsteady-state and steady-state energy balances.
 - - Identify and evaluate multiple steady states in CSTRs.
 - - Apply ignition and extinction concepts to reactor design.

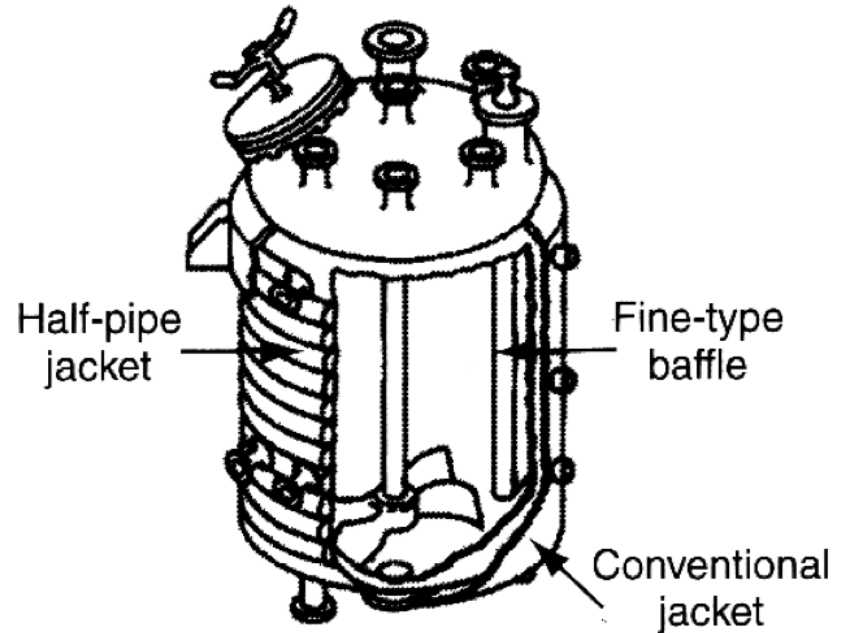
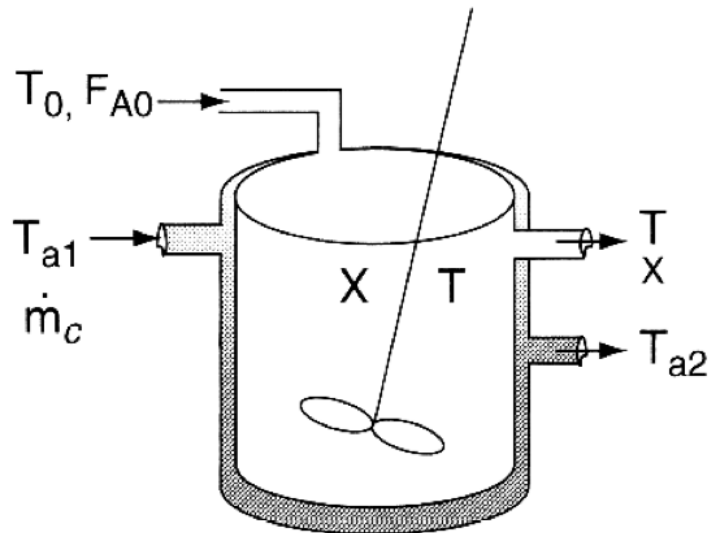
Introduction

- Understanding the relationship between heat generation and removal is crucial for predicting reactor stability.
- This session delves into steady-state and unsteady-state energy balances, multiple steady states, and the associated temperature profiles.

CSTR with Heat Effects



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Courtesy of Pfaudler, Inc.

Unsteady State Energy Balance



$$\dot{Q} - \dot{W}_S + \sum_{i=1}^n F_{i0} H_{i0} - \sum_{i=1}^n F_i H_i = \frac{d\hat{E}_{\text{sys}}}{dt}$$

Neglect

Using $\hat{E}_{\text{sys}} = \sum N_i E_i = \sum N_i (H_i - PV_i) = \sum N_i H_i - P \cancel{V}$

$$\frac{dE_{\text{sys}}}{dt} = \frac{d \sum N_i H_i}{dt} = \sum N_i \frac{dH_i}{dt} = \sum H_i \frac{dN_i}{dt}$$

$$\frac{dH_i}{dt} = C_{Pi} \frac{dT}{dt}$$

$$\frac{dN_i}{dt} = -v_i r_A V + F_{i0} - F_i$$

We obtain after some manipulation:

$$\frac{dT}{dt} = \frac{\dot{Q} - \dot{W}_S - \sum F_{i0} C_{Pi} (T - T_{i0}) + [-\Delta H_{Rx}(T)](-r_A V)}{\sum N_i C_{Pi}}$$

Collecting terms with $\dot{Q} = UA(T_a - T)$ and $\dot{W}_S = 0$ high coolant flow rates, and $F_{i0} = F_{A0} \Theta_i$

$$\frac{dT}{dt} = \frac{(\Delta H_{RX})(r_A V) - \left[F_{A0} \overbrace{\sum \Theta_i C_{P_i}}^{C_{P_0}} (T - T_0) + (UA(T - T_a)) \right]}{\sum N_i C_{P_i}}$$

$$= \frac{F_{A0}}{\sum N_i C_{P_i}} \left[\overbrace{\Delta H_R \frac{r_A V}{F_{A0}}}^{G(T)} - \overbrace{\left[C_{P_0} \left[T - T_0 + \frac{UA}{\underbrace{F_{A0} C_{P_S}}_{\kappa}} (T - T_a) \right] \right]}^{R(T)} \right]$$

$$\frac{dT}{dt} = \frac{F_{A0}}{\sum N_i C_{P_i}} [G(T) - R(T)]$$

$$G(T) = (r_A V) [\Delta H_{R_x}]$$

$$R(T) = C_{P_0} [(1 + \kappa)T - (T_0 + \kappa T_a)]$$

$$R(T) = C_{P_0} (1 + \kappa) \left(T - \frac{T_0 + \kappa T_a}{1 + \kappa} \right) = C_{P_0} (1 + \kappa) (T - T_C)$$

$$\kappa = \frac{UA}{F_{A0} C_{P0}}$$

$$T_C = \frac{T_0 + \kappa T_a}{1 + \kappa}$$

$$\frac{dT}{dt} = G(T) - R(T)$$

If $G(T) > R(T)$ Temperature Increases

If $R(T) > G(T)$ Temperature Decreases

At Steady State

$$\frac{dT}{dt} = \frac{dN_A}{dt} = 0$$

$$-r_A V = F_{A0} X$$

$$G(T) - R(T) = 0$$

$$(-\Delta H_{RX})F_{A0}X - F_{A0} \sum \Theta_i C_{P_i} (T - T_0) - UA(T - T_a) = 0$$

Solving for X.

Solving for X:

$$X = \frac{\sum \Theta_i C_{P_i} (T - T_0) + \frac{UA}{F_{A0}} (T - T_a)}{-\Delta H_{Rx}^\circ} = X_{EB}$$

Solving for T:

$$T = \frac{F_{A0} X (-\Delta H_{Rx}) + UA T_a + F_{A0} \sum \Theta_i C_{P_i} T_0}{UA + F_{A0} \sum \Theta_i C_{P_i}}$$

Steady State Energy Balance for CSTRs



$$X(-\Delta H_{RX}) = C_{P_0} \left[T - T_0 + \frac{UA}{F_{A0}C_{P_0}} (T - T_a) \right]$$

$$\text{Let } \kappa = \frac{UA}{F_{A0}C_{P_0}}$$

$$\begin{aligned} X(-\Delta H_{RX}) &= C_{P_0} (T + \kappa T - T_0 - \kappa T_a) = C_{P_0} (1 + \kappa) \left(T - \frac{T_0 + \kappa T_a}{1 + \kappa} \right) \\ &= C_{P_0} (1 + \kappa) (T - T_C) \end{aligned}$$

$$T_C = \frac{T_0 + \kappa T_a}{1 + \kappa}$$



$$\overbrace{-X \Delta H^{\circ}_{Rx}}^{G(T)} = \overbrace{C_{p0}(1+\kappa)(T-T_C)}^{R(T)}$$

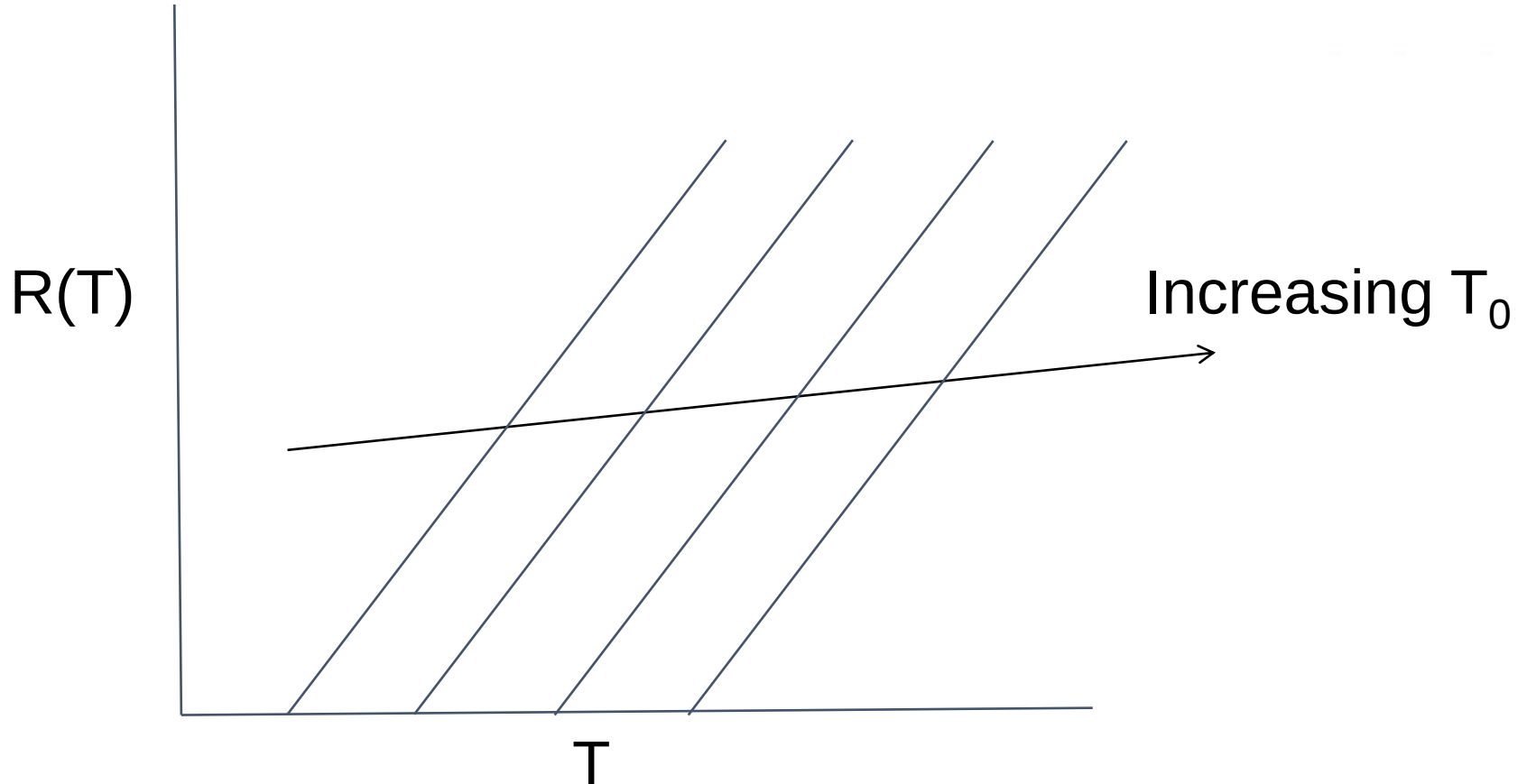
$$X = \frac{C_{p0}(1+\kappa)(T-T_C)}{-\Delta H^{\circ}_{Rx}}$$

$$T = T_C + \frac{(-\Delta H^{\circ}_{Rx})(X)}{C_{p0}(1+\kappa)}$$

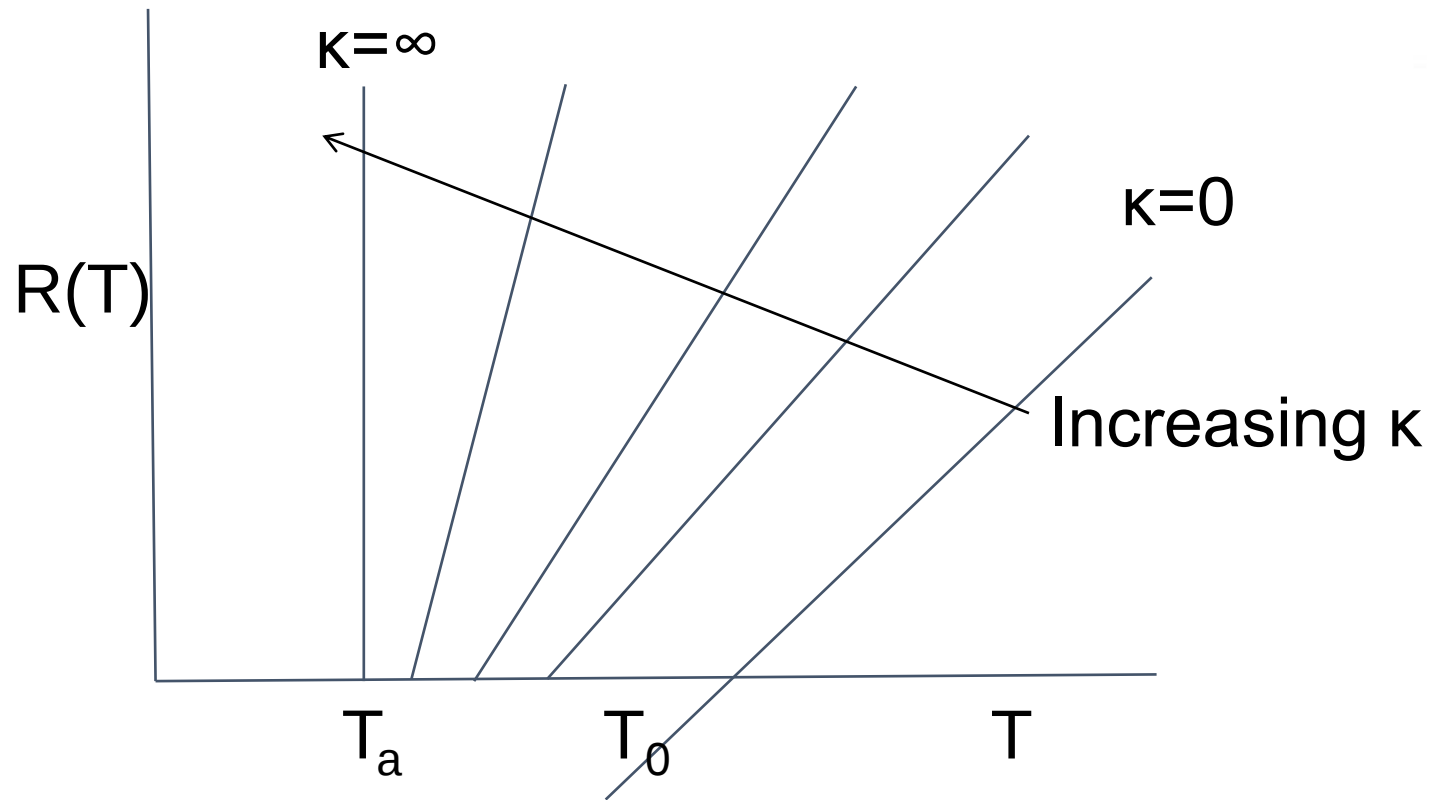
Steady State Energy Balance for CSTRs



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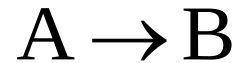


Variation of heat removal line with inlet temperature.



Variation of heat removal line with κ ($\kappa=UA/C_{P0}F_{A0}$)

$$V = \frac{F_{A0}X}{-r_A(X, T)}$$



1) Mole Balances:

$$V = \frac{F_{A0}X}{-r_A}$$

2) Rate Laws:

$$-r_A = kC_A$$

3) Stoichiometry:

$$C_A = C_{A0}(1 - X)$$

4) Combine:

$$V = \frac{F_{A0}X}{kC_{A0}(1 - X)} = \frac{C_{A0}v_0X}{kC_{A0}(1 - X)}$$

$$\tau k = \frac{X}{1 - X}$$

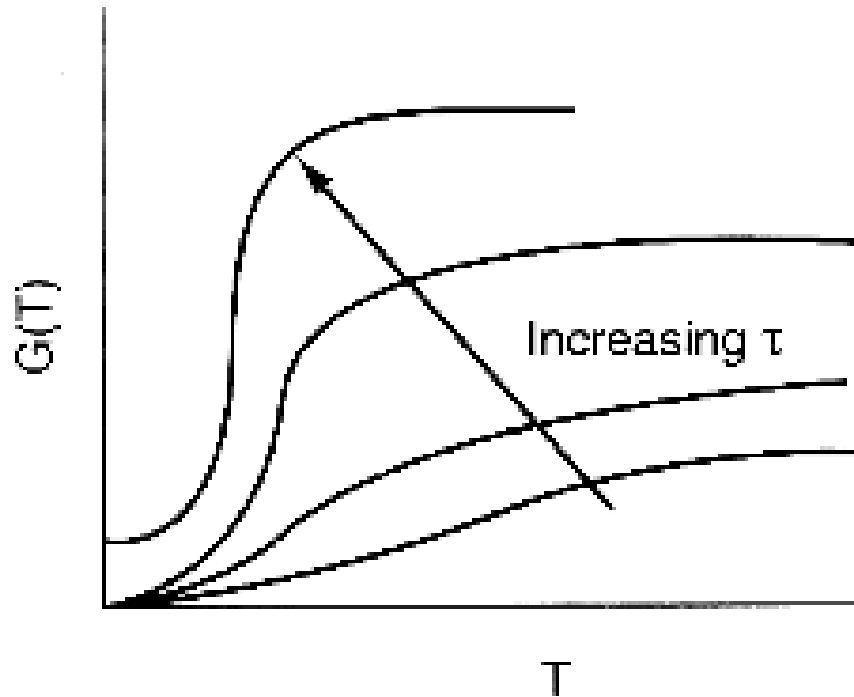
$$X = \frac{\tau k}{1 + \tau k} = \frac{\tau A e^{-E/RT}}{1 + A e^{-E/RT}}$$

$$G(T) = X(-\Delta H_{Rx}) = \frac{\tau A e^{-E/RT}}{1 + A e^{-E/RT}} (-\Delta H_{Rx})$$

Multiple Steady States (MSS)



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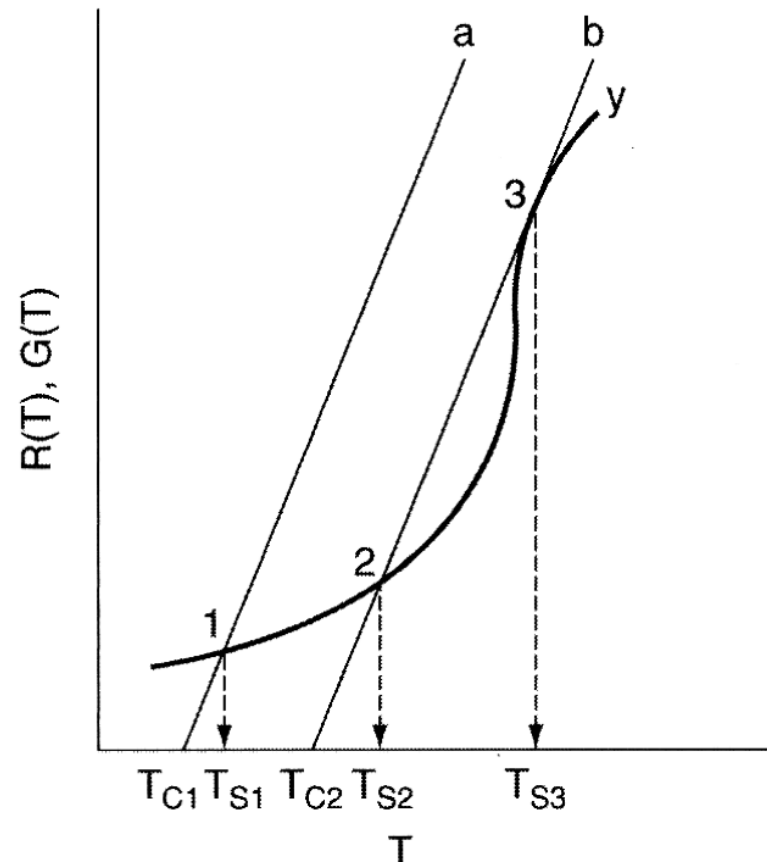


Variation of heat generation curve with space-time.

Multiple Steady States (MSS)



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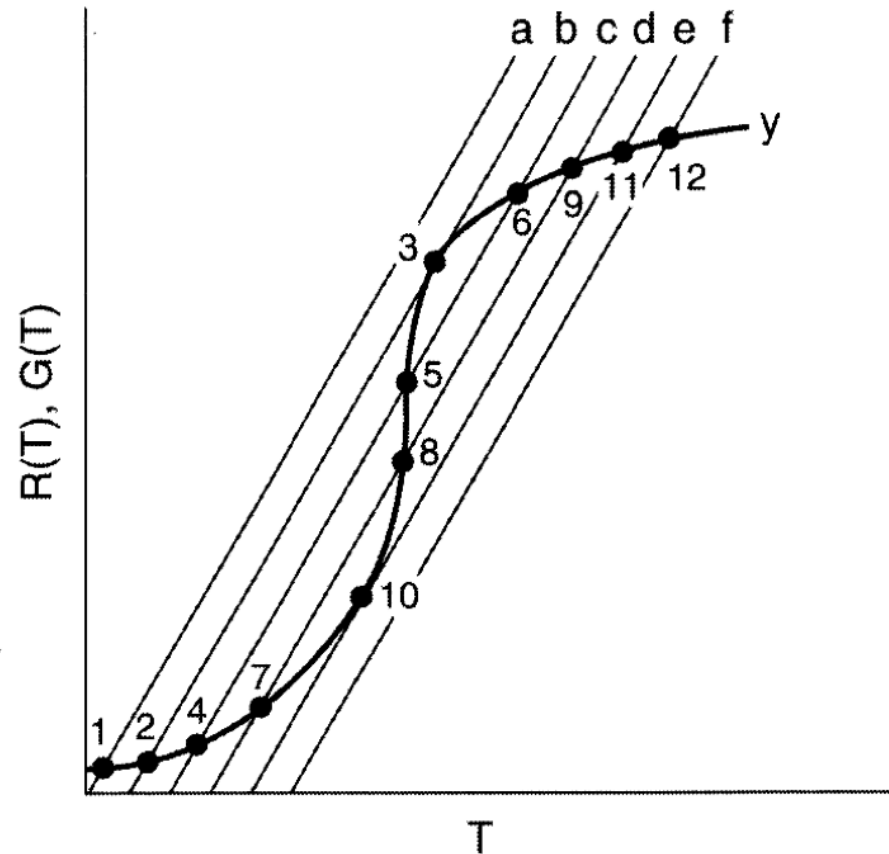


Finding Multiple Steady States with T_0 varied

Multiple Steady States (MSS)



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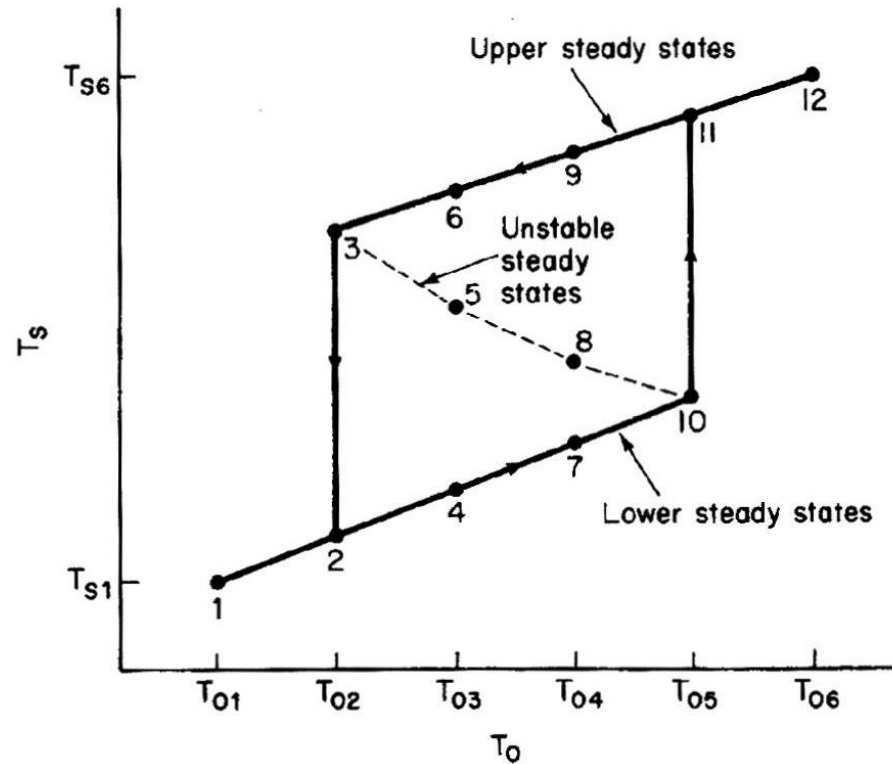


Finding Multiple Steady States with T_0 varied

Multiple Steady States (MSS)



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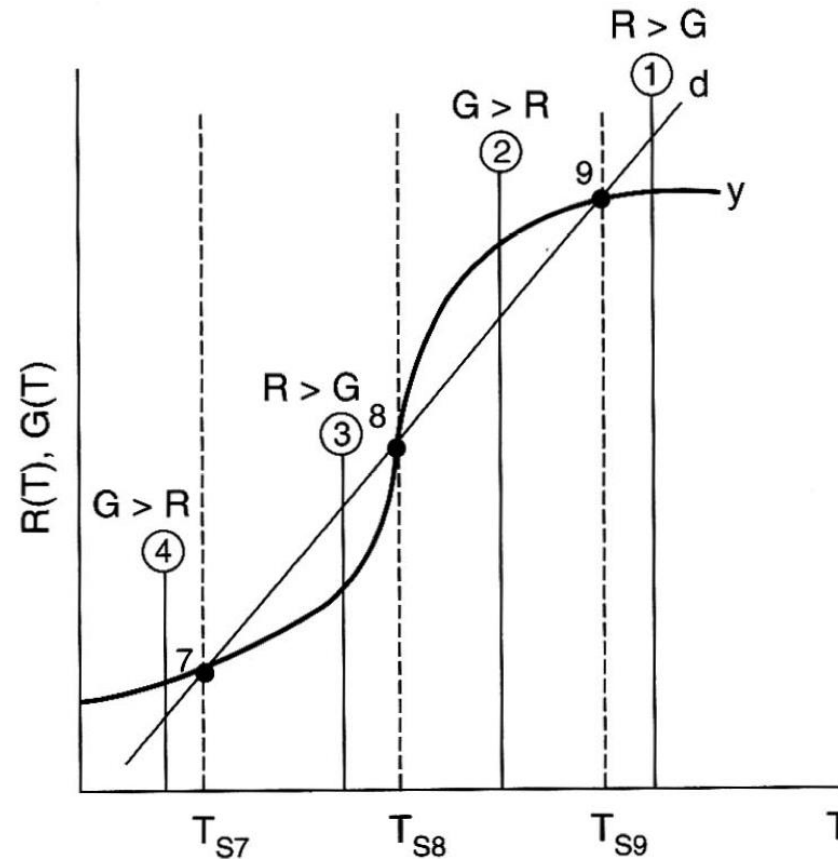


Temperature ignition-extinction curve

Multiple Steady States (MSS)



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Stability of multiple state temperatures

$$\frac{dT}{dt} = 1$$

$$G(T) = X \cdot (-\Delta H_{Rx})$$

$$R = C_{P_0} \cdot (1 + \kappa) \cdot (T - T_C)$$

Need to solve for X after combining **mole balance**, **rate law**, and **stoichiometry**.

MSS - Generating G(T) and R(T)



For a first order irreversible reaction

$$X = \frac{\tau \cdot k}{(1 + \tau \cdot k)}$$

$$k = k_1 \exp \left[\frac{E}{R} \left(\frac{1}{T_1} - \frac{1}{T} \right) \right]$$

Parameters

$\tau, (-\Delta H_{RX}), k_1, E, R, T_1, T_C, \kappa, C_{P_0}$

Then plot G and R as a function of T.

Are you ready?



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Summary

- In this lecture, we covered:
 - - Heat effects and energy balance fundamentals for CSTRs.
 - - Analysis of multiple steady states and their stability.
 - - Concepts of ignition and extinction temperatures.
 - - Practical examples to reinforce theoretical concepts.
- Understanding these principles is critical for designing stable and efficient reactor systems.